



# CHICAGO

2024 WINTER CONFERENCE  
AND AHR EXPO

January 20–24, 2024

Seminar 31 - Monday, January 22

## Heat Pumps: a High Potential Solution to Decrease Operational CO<sub>2</sub> Emissions in Buildings



**Cătălin Lungu**

President

Mandate: 2022 – 2025



Apartment Building    Corporate Building    Industrial Site    Hospital    Mall    Hotel    Congress Center & Institution    Cinema Theater    Airport



# LERNING OBJECTIVES AND DISCLAIMER

## Learning Objectives:

- Describe the main indicator used in Europe to assess the Building Global Warming Potential
- Explain the main indicators used in Europe to measure energy performance of buildings
- Compare and contrast the outcomes of three common primary energy indicator calculation approach
- Explain the meaning of on-site renewable energy generation and ambient heat in the primary energy calculation

## ASHRAE disclaimer:

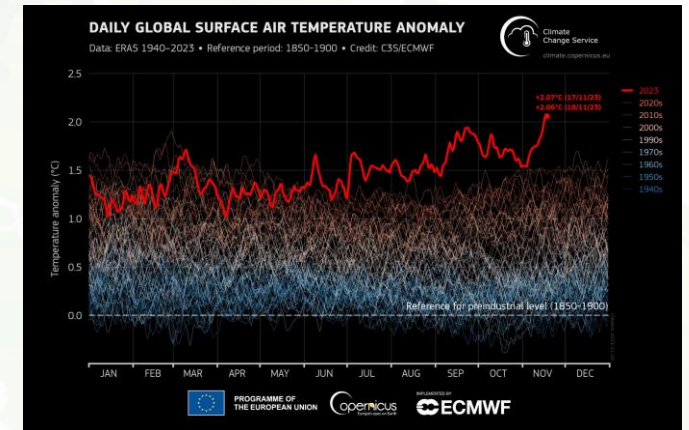
ASHRAE is a Registered Provider with the American Institute of Architects Continuing Education Systems. Credit earned on completion of this program will be reported to ASHRAE Records for AIA members. Certificates of Completion for non-AIA members are available on request.

This program is registered with the AIA/ASHRAE for continuing professional education. As such, it does not include content that may be deemed or construed to be an approval or endorsement by the AIA or any material of construction or any method or manner of handling, using, distributing, or dealing in any material or product. Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.

# 1. PREAMBULE

## Is anyone in the room against decarbonization / sustainability ?

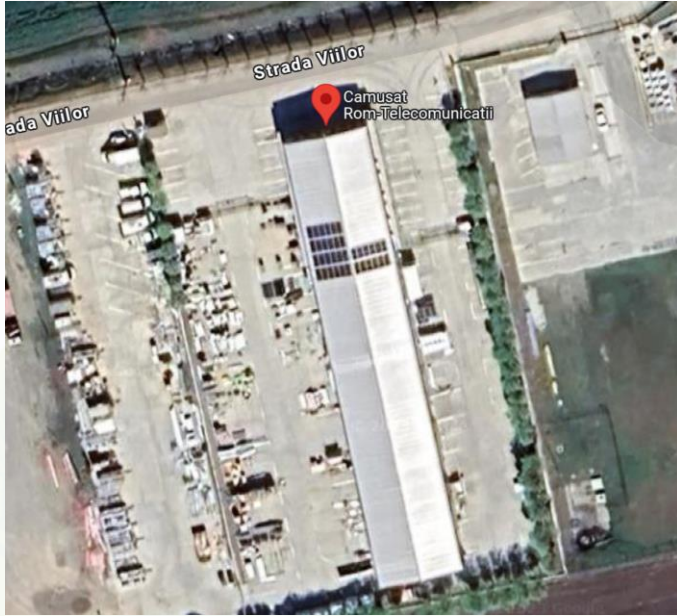
- 17<sup>th</sup> of Nov - the first day when global temperature was more than 2°C above 1850-1900 (or pre-industrial) levels, at 2,06°C (source Copernicus)



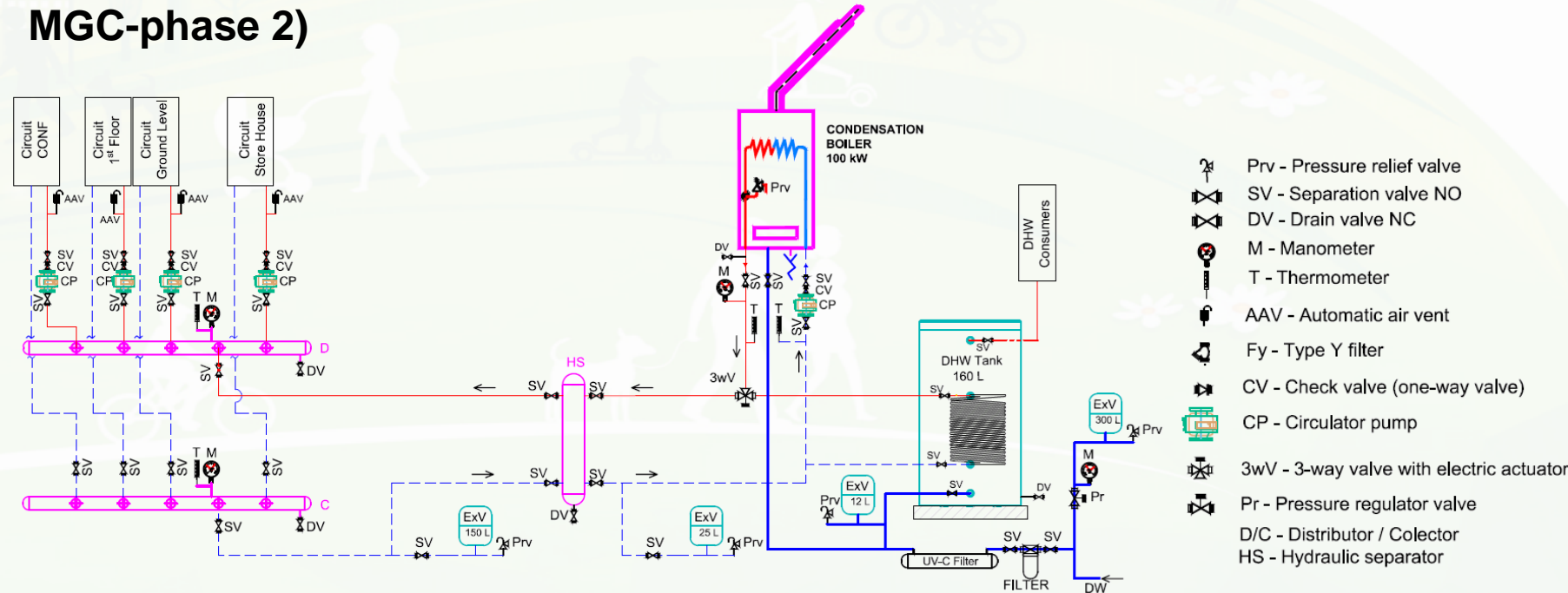
- even if all NDCs will be respected, the global CO<sub>2</sub> emissions +9%/2030 vs 2010, -2%/2030 vs 2019 compared with the reduction needed -43%/2030 vs 2019 (ie max +1,5°C) (source IPCC)

# 2. HVAC system design - problem definition

Source: google maps



- office building (1250 m<sup>2</sup>) + storing house (250 m<sup>2</sup>), near Bucharest, G+1 floor
- roof – sandwich pannels Lindab Roof of 60 mm, walls – sandwich Lindab Wall of 80 mm (polyurethane), fenestration – Al profiles and low-e double glazing
- Heating+DHW with NG boiler 100 kW, cooling with split 40kW (27pcs A/C), PV pannels (19,44 kWp, 36 pcs, 540 Wp, ε=up to 20%)
- **MAIN OBJECTIVE:** replace the boiler with heat pump(s) & find the optimal solution out of min 3 choices (i.e. find min delivered energy–phase 1 and MGC-phase 2)



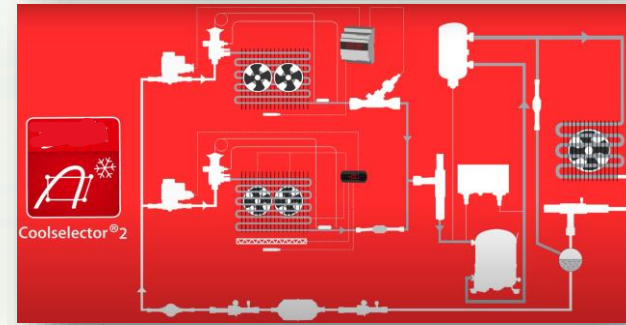
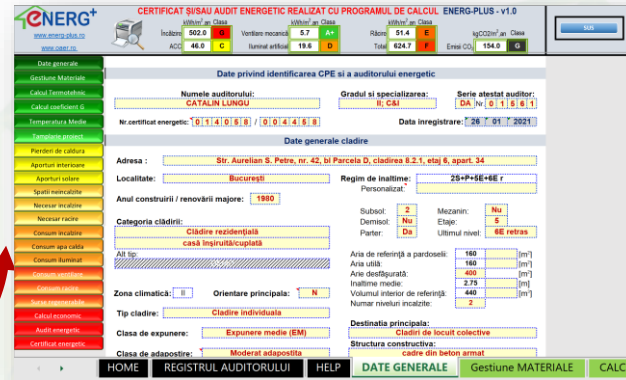
# 3. HVAC system design - optimization procedure

1 Collect data (measured and rated monthly average outside temperature - ex METEONORM, measured delivered energy for H/C/DHW/L/V) and adjust measured energy consumption

2 Estimate by calculation the heating/cooling season [ENERG+]

3 Normalize the monthly values of the measured delivered energy (heating/cooling), using DD method (winter and summer)

4 Select different options of HPs and HVAC systems (min3)



5 Use COOLSELECTOR2 to estimate the theoretical COP/EER for real COP/EER (values from catalogue)

6 Find the regression equation for each HP and compute real monthly average COP/EER function of standard values of the monthly average outside temperature

7 Compute the electric energy consumption delivered by the grid or by a mixture grid-PV + use PVSYS



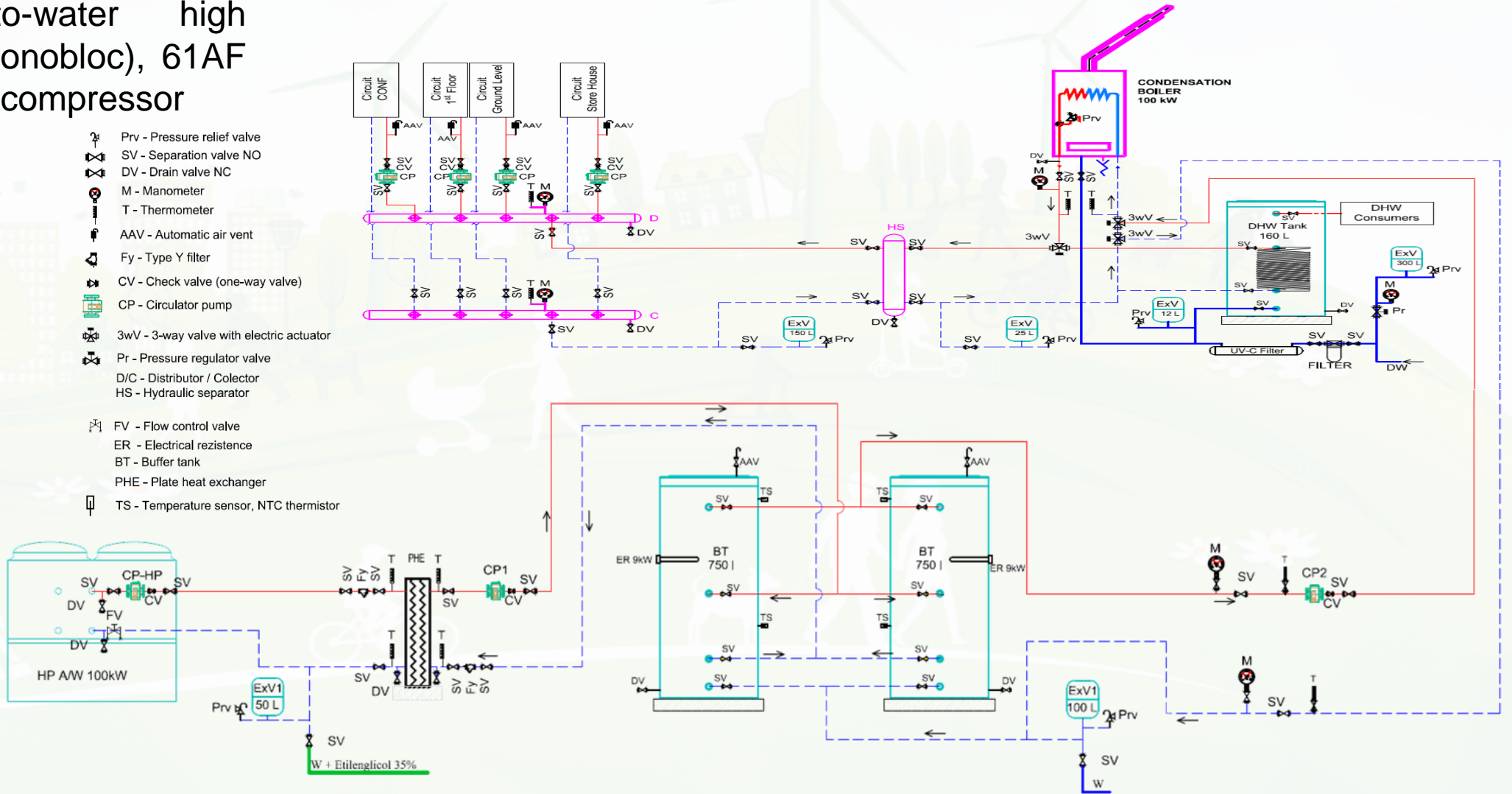
8 Compute the primary energy consumption and the CO<sub>2</sub>e emissions

# 3. HVAC system design - optimization procedure

**CASE 1:** Air-to-water high temperature HP (monobloc), 61AF105, R-407C, scroll compressor

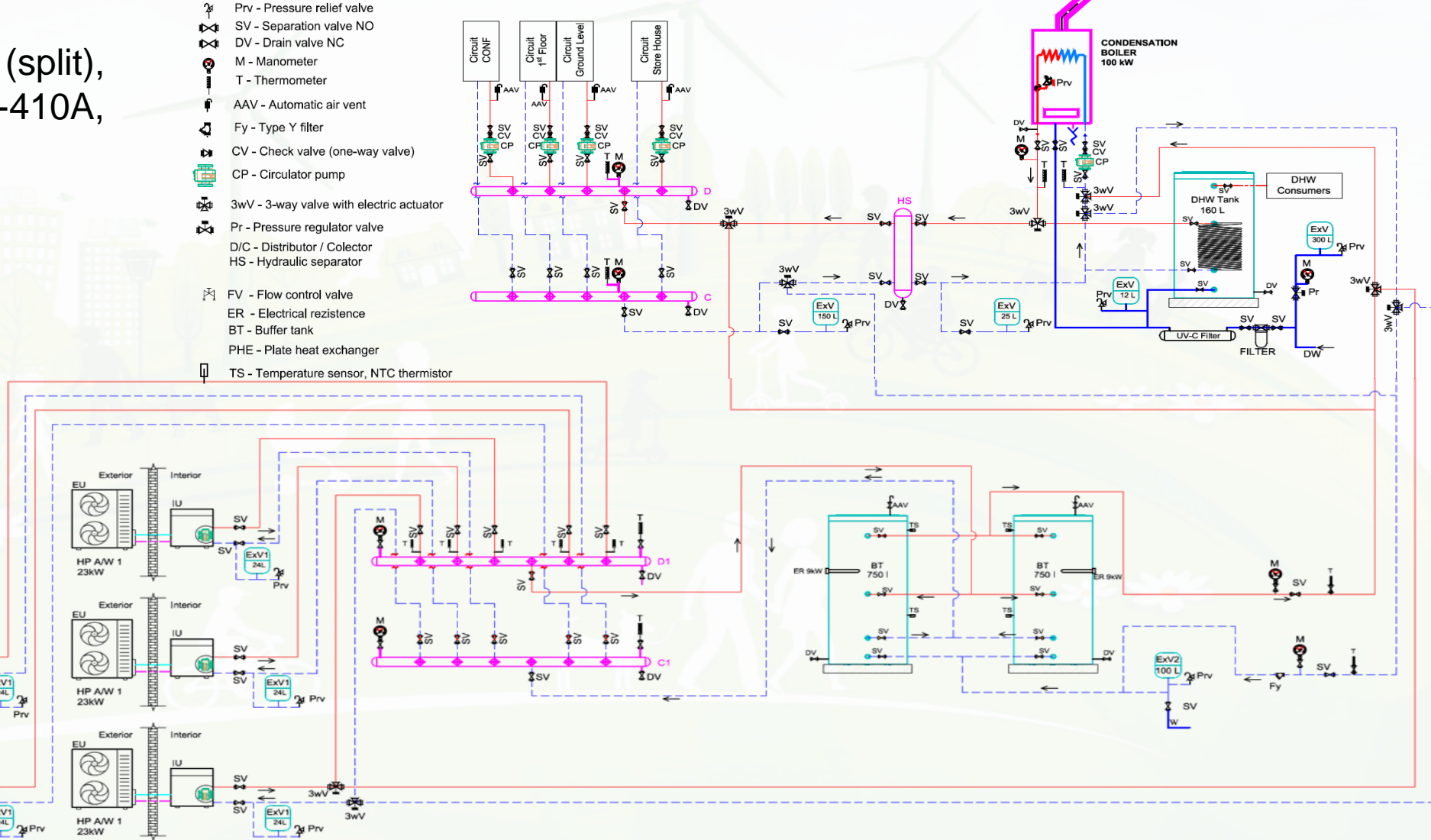
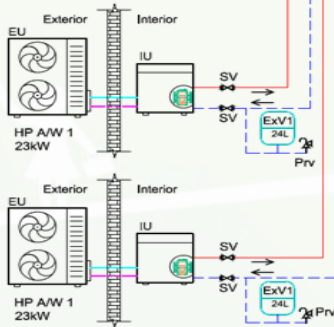


- Prv - Pressure relief valve
- SV - Separation valve NO
- DV - Drain valve NC
- M - Manometer
- T - Thermometer
- AAV - Automatic air vent
- Fy - Type Y filter
- CV - Check valve (one-way valve)
- CP - Circulator pump
- 3wV - 3-way valve with electric actuator
- Pr - Pressure regulator valve
- D/C - Distributor / Colector
- HS - Hydraulic separator
- FV - Flow control valve
- ER - Electrical resistence
- BT - Buffer tank
- PHE - Plate heat exchanger
- TS - Temperature sensor, NTC thermistor



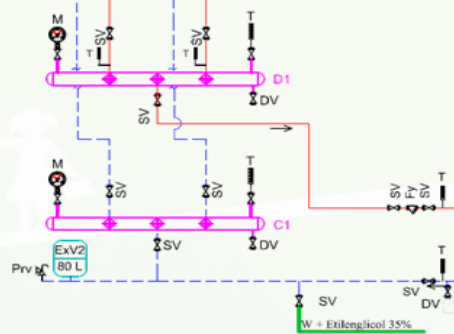
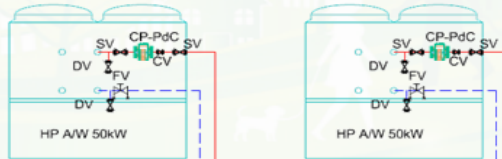
# 3. HVAC system design - optimization procedure

**CASE 2: Air-to-water HP (split), PUAZ-SHW230YKA2, R-410A, injection compressor**

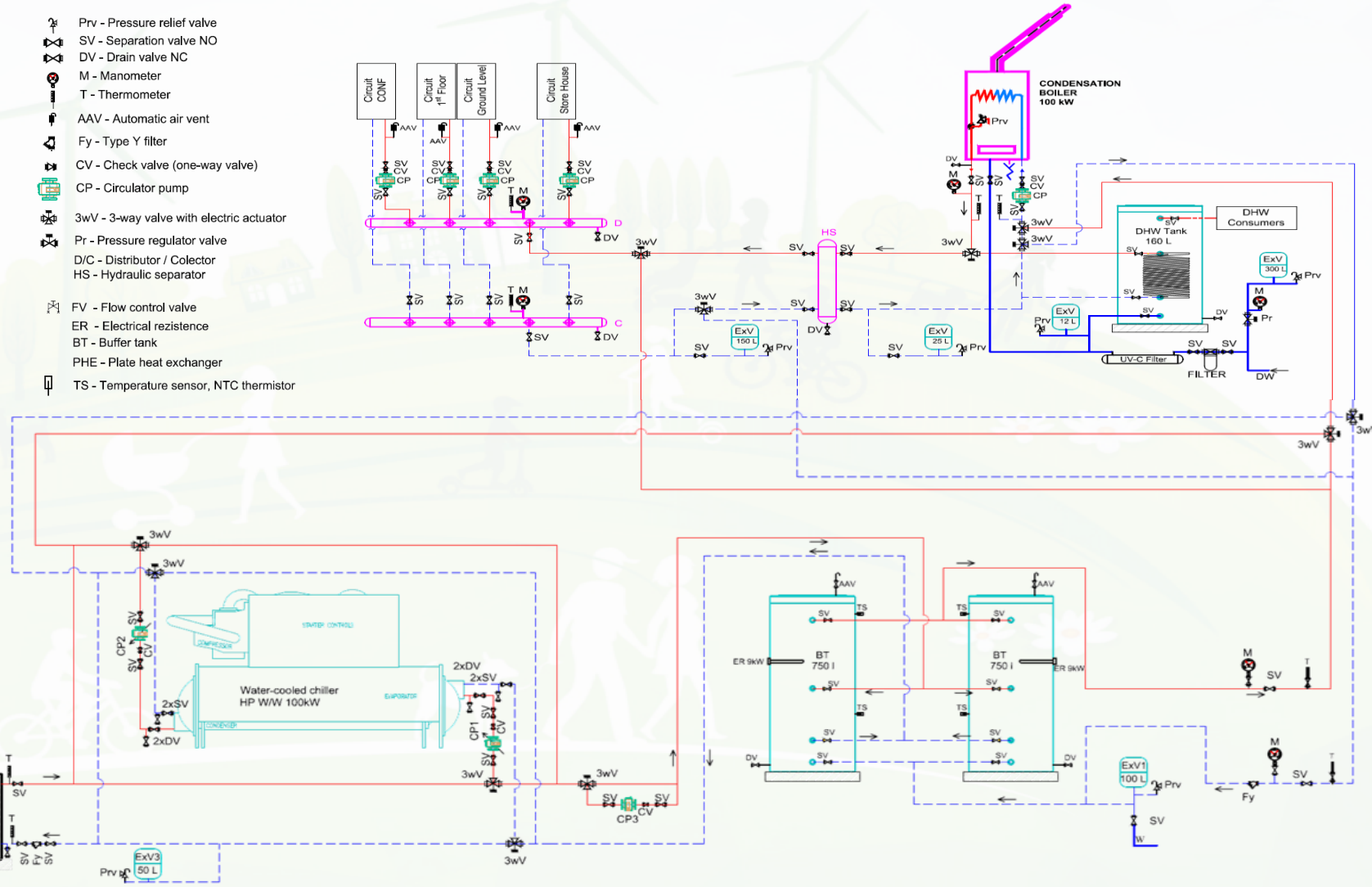


# 3. HVAC system design - optimization procedure

## CASE 3: Air-to-water + water-to-water HP, cascade



- Prv - Pressure relief valve
- SV - Separation valve NO
- DV - Drain valve NC
- M - Manometer
- T - Thermometer
- AAV - Automatic air vent
- Fy - Type Y filter
- CV - Check valve (one-way valve)
- CP - Circulator pump
- 3wV - 3-way valve with electric actuator
- Pr - Pressure regulator valve
- D/C - Distributor / Collector
- HS - Hydraulic separator
- FV - Flow control valve
- ER - Electrical resistance
- BT - Buffer tank
- PHE - Plate heat exchanger
- TS - Temperature sensor, NTC thermistor

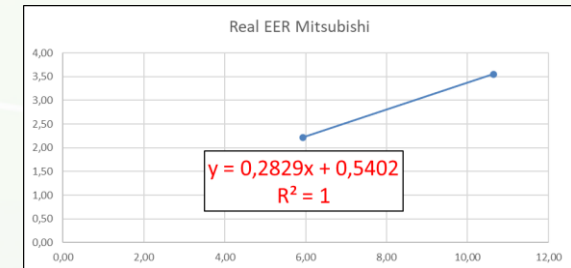
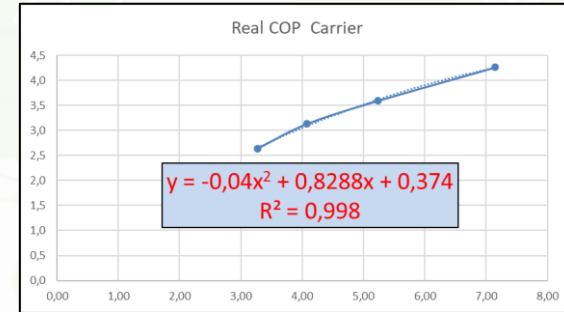




# 3. HVAC system design - optimization procedure

| Heat Pump Producer & short description  | Heat Pump Code  | Refrigerant type | Rated Heating Capacity [kW] | COP W35/A7 | COP W45/A7 | COP W55/A7 | COP W65/A7 | Rated Cooling Capacity [kW] | EER (A35/W7) | EER (A35/W18) |
|---|-----------------|------------------|-----------------------------|------------|------------|------------|------------|-----------------------------|--------------|---------------|
| CARRIER, high-temperature monobloc air-to-water heat pumps with integrated hydraulic module, scroll compressors, -20/65grdC | 61AF 105        | R-407C           | 102                         | 4.26       | 3.59       | 3.13       | 2.64       | -                           | -            | -             |
| mitsubishi, air-to-water heat pump, split type, Zubadan injection compressor, -25/65grdC                                    | PUHZ-SHW230YKA2 | R410A            | 23                          | 3.65       | 3,02       | 2,47       | -          | 20                          | 2,22         | 3,55          |
| MAXA, reversible inverter heat pump with steam injection, scroll compressors  | i-HP/LT 0250    | R410A            | 47,78                       | 3,93       | 3,33       | -          | -          | 36,1                        | 2,9          | 3,8           |
| TRANE, water to water heat pumps, helical-rotary compressor   | RTSF 050 G      | R1234ze          | 204                         | 5,75       | 4,5        | 3,74       | 3,02       | 184                         | 5,03         | -             |

| Month | Θ [grdC] standardized | COP    |        |         |         | EER    |        |        |
|-------|-----------------------|--------|--------|---------|---------|--------|--------|--------|
|       |                       | Case 1 | Case 2 | Case 3  |         | Case 1 | Case 2 | Case 3 |
|       |                       |        |        | Stage 1 | Stage 2 |        |        |        |
| Jan   | -1,2                  | 2,45   | 1,78   | 3,50    | 4,69    | 2,9    | -      | -      |
| Feb   | 1,2                   | 2,53   | 1,87   | 3,66    | 4,69    | 2,9    | -      | -      |
| March | 5,6                   | 2,57   | 1,92   | 3,74    | 4,69    | 2,9    | -      | -      |
| April | 11,3                  | 2,74   | 2,12   | 4,16    | 4,69    | 2,9    | -      | 5,37   |
| May   | 17,5                  | 2,78   | 2,15   | -       | -       | 2,9    | 5,86   | 4,26   |
| June  | 21,4                  | 2,78   | 2,15   | -       | -       | 2,9    | 4,23   | 3,66   |
| July  | 23,4                  | 2,78   | 2,15   | -       | -       | 2,9    | 3,35   | 3,61   |
| Aug   | 22,5                  | 2,78   | 2,15   | -       | -       | 2,9    | 3,29   | 4,88   |
| Sept  | 16,8                  | 2,78   | 2,15   | -       | -       | 2,9    | 5,14   | -      |
| Oct   | 11,1                  | 2,78   | 2,15   | 4,25    | 4,69    | 2,9    | -      | -      |
| Nov   | 5,2                   | 2,66   | 2,15   | 3,95    | 4,69    | 2,9    | -      | -      |
| Dec   | -0,2                  | 2,49   | 2,02   | 3,58    | 4,69    | 2,9    | -      | -      |

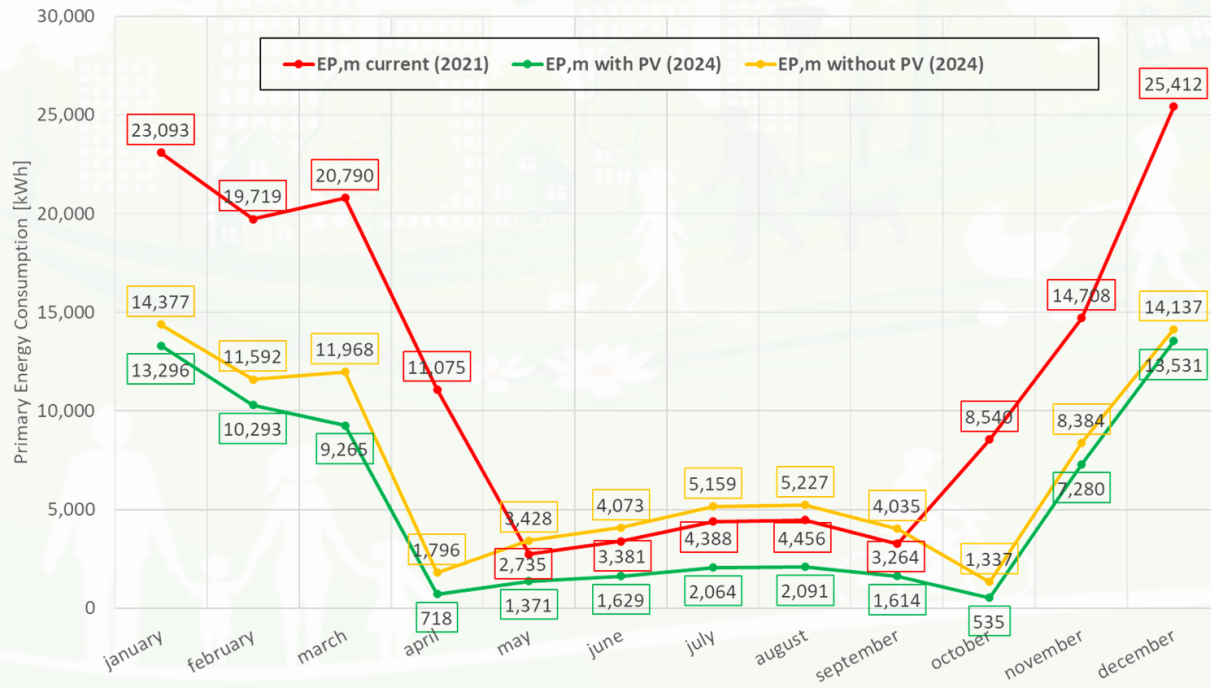


# 4. Results

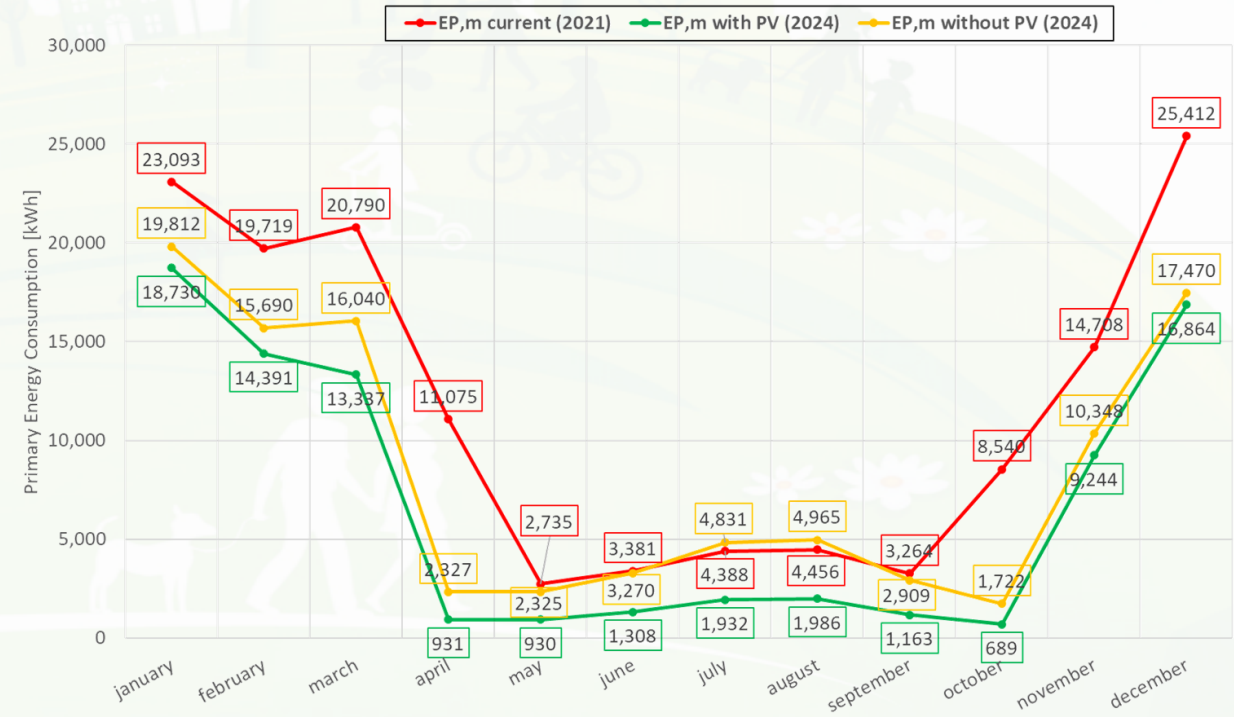
**CASE 1 – monobloc HP (1pc)**  
**-23%/-57% PE & -37/-68% CO<sub>2</sub>e, yearly**

**CASE 2 – split air-to-water HPs (5 pcs)**  
**-24%/-53% PE & -41/-68% CO<sub>2</sub>e, yearly**

Primary Energy 2021 vs. 2024 - MONOBLOC



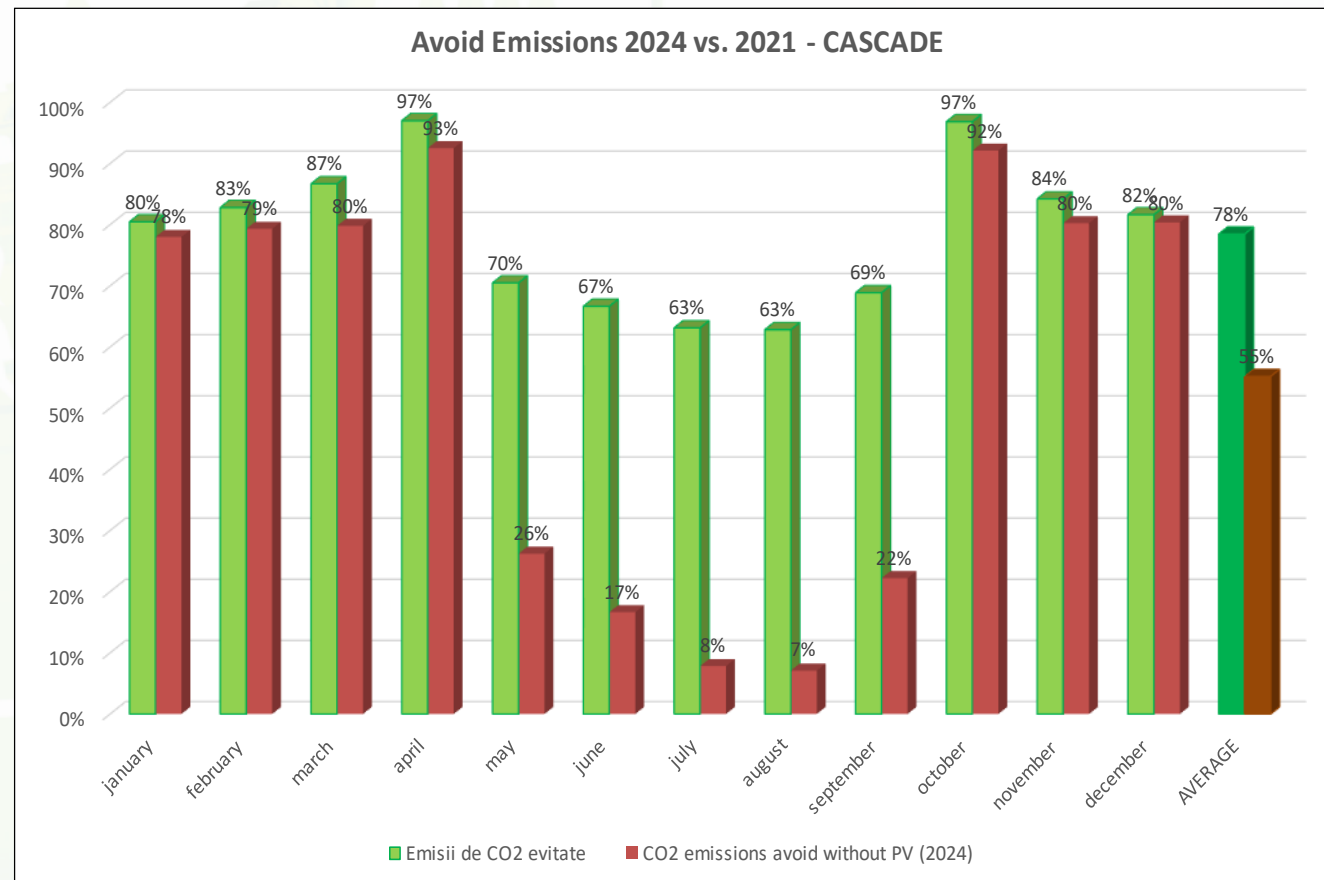
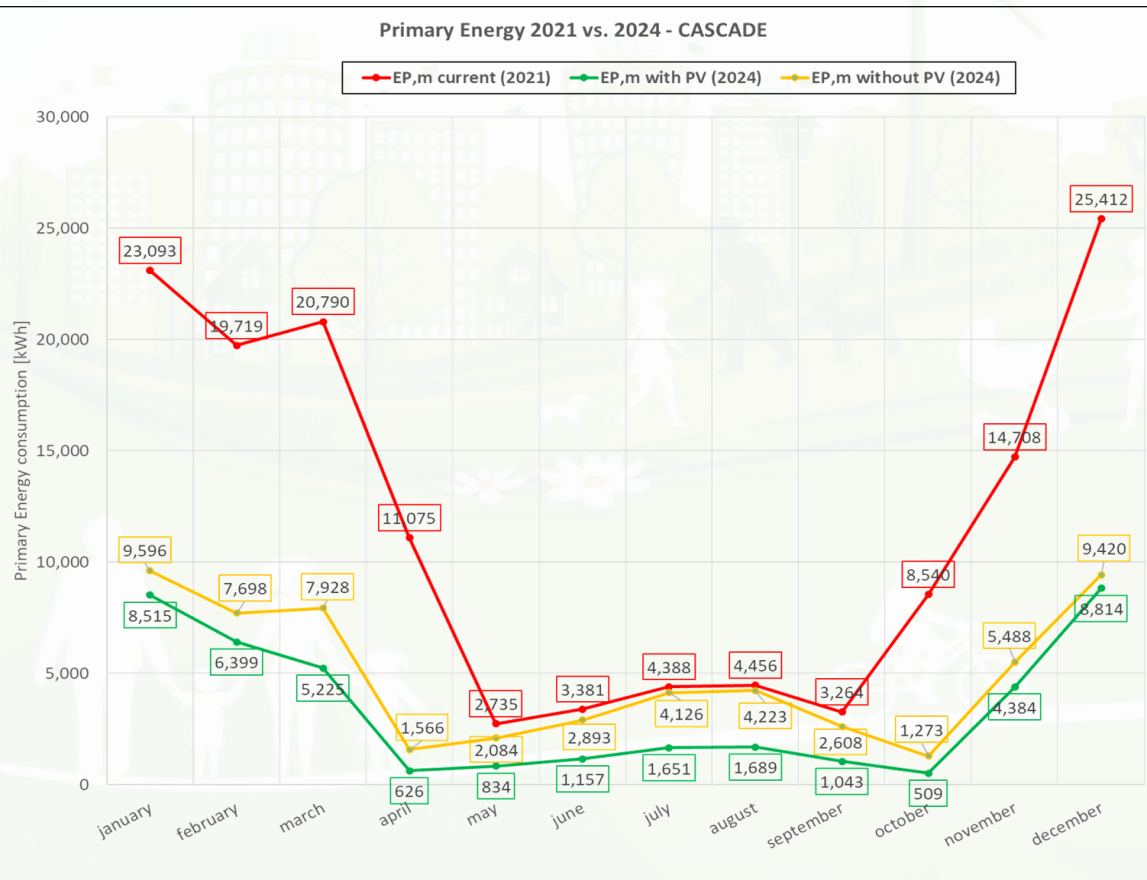
Primary Energy 2021 vs. 2024 - SPLIT



# 4. Results

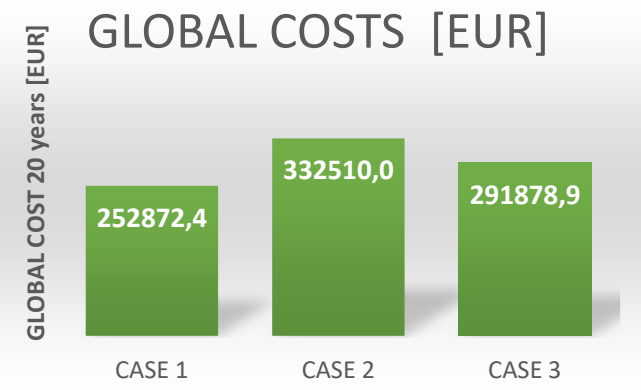
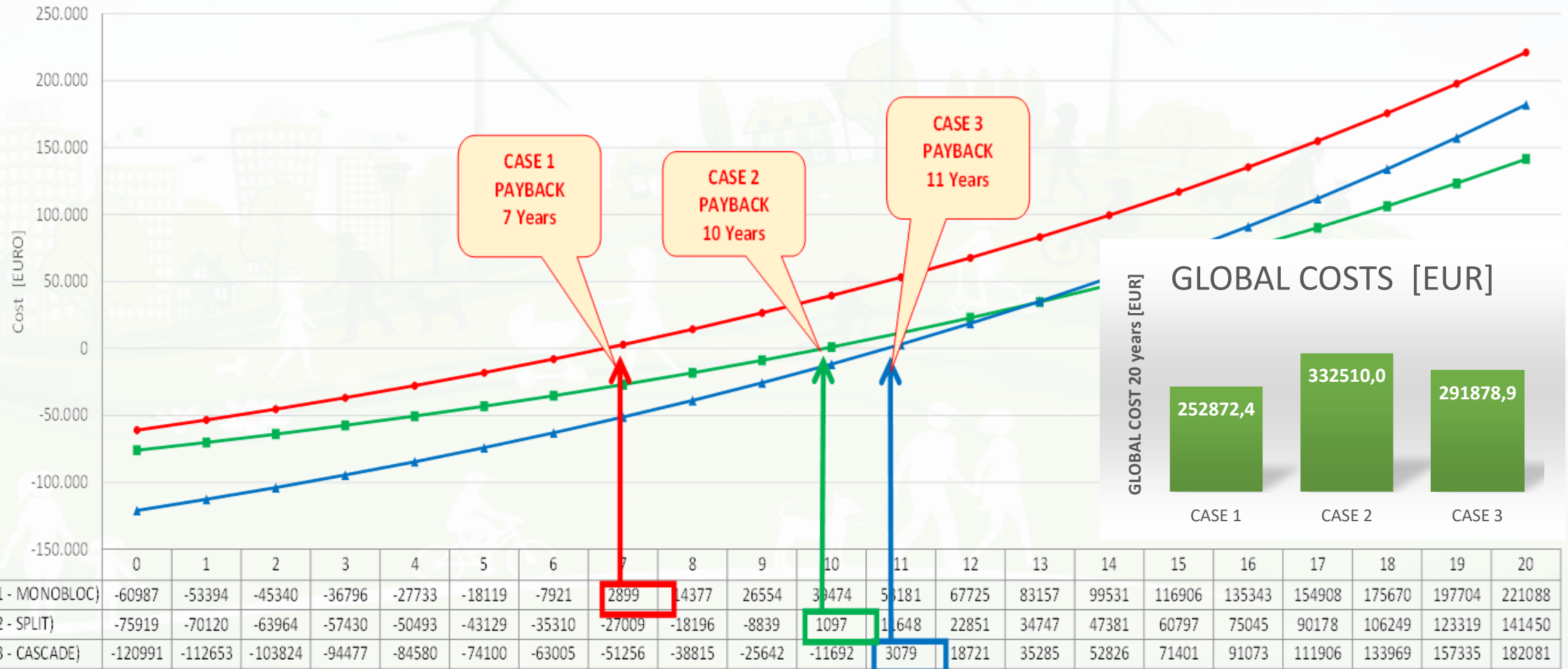
## CASE 3 – cascade HP system -46%/-71% annual EP

## CASE 3 – cascade HP system -55%/-78% avoided CO<sub>2</sub>e, yearly



# 4. Results

CUMULATIVE CASH FLOW - PAYBACK PERIOD (COMPARISON)



# 5. Conclusions and perspectives

- ❖ No building renovation before boiler replacement (usual case with minimum investment)
- ❖ The current procedure – based on simplified hypothesis (calculated number of operating days and constant COP/EER per month etc.)
- ❖ Monthly calculation using EPB standards (perspective-implementing an hourly method)
- ❖ HP can benefit from existing PV, but even without PV the replacement was profitable
- ❖ This procedure – a first step for an automated calculation procedure to find the OGC for NZEB or for refurbished buildings
- ❖ Further investigations for higher heating and cooling capacities



SHARE/

Submit a Manuscript to the Journal

International Journal of Sustainable Energy

For an Article Collection on

Advancing Net-Zero and Zero-Energy Buildings: Challenges and Opportunities in Sustainable Design and Operation

Manuscript deadline  
31 May 2024

OPEN  ACCESS

Questions ?  
Thank you !



**SAVE THE EARTH !**

Associate Professor Cătălin Lungu, PhD  
[president@rehva.eu](mailto:president@rehva.eu), [catalin.lungu@utcb.ro](mailto:catalin.lungu@utcb.ro)